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13. ABSTRACT (Maximum 200 words) THE NEED TO FIND KINETIC RATE CONSTANTS FOR SELECTED ALUMINAS WAS GENERATED FROM PREVIOUS ALUMINA COLUMN STUDIES PERFORMED AT ROCKY MOUNTAIN ARSENAL. THE PROBLEM THAT HAD NOT BEEN ADDRESSED WAS FINDING A MEANS OF CALCULATING THE INITIAL FLUORIDE REMOVAL BY ALUMINAS BEFORE THE LINEAR PORTION OF THE FLUORIDE BREAK-THROUGH CURVE HAD BEEN REACHED SIX ALUMINAS WERE CHOSEN FOR PSEUDO-KINETIC RATE CONSTANT TEST RUNS. EXPERIMENTAL AND MATHEMATICAL METHODOLOGY ARE GIVEN IN THE PROCEDURE SECTION.		

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ARE MISSING.**

JANUARY 31, 1996

DRAFT

TEST ON SELECTED ALUMINAS TO DETERMINE

PSUEDO-KINETIC RATE CONSTANTS AND CHARACTERIZE ADSORPTION CURVES

IN SUPPORT OF ITARMS TASK NO. 10595

BY

DENNIS M. PRUSINSKI, Ch. E., P. D & E, C.M., RMA

ROCKY MOUNTAIN ARSENAL
COMMERCE CITY, CO 80022

JULY 1979

APPROVAL:

CARL G. LOVEN
Chemical Engineer
Process Development and Engineering Branch
Industrial Division

Class
Don Campbell
original
81325R20
Rocky Mountain Arsenal
Information Center
Commerce City, Colorado

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PURPOSE

The tests performed prior to this test run established the technical and economic feasibility of efficient fluoride removal via alumina column adsorption. This followed with second generation research effort that has or is being completed on aluminas column adsorption modes, but the derivation of a predictive mathematical model for alumina columns had not been made. These tests were made to find a predictive mathematical model for alumina columns. This predictive model uses a psuedo-kinetic rates constant, rate expression which enables alumina column behavior to be predicted for selected aluminas. The predicted behavior (theoretical) can then be compared to the actual behavior to determine if the actual behavior follows the predictive behavior. Significant deviations would indicate either an alumina column plant malfunction and/or misadjusted; thus an early diagnosis (warning) could be made of plant failure and subsequent fix would greatly shorten downtime and improve the overall plant efficiency.

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DETERMINATION OF KINETIC RATE CONSTANTS IN ALUMINA ADSORPTION FOR SELECTED ALUMINAS

INTRODUCTION

The need to find kinetic rate constants for selected aluminas was generated from the alumina column test results at Rocky Mountain Arsenal. The problem that had not been addressed was finding a means of calculating the initial fluoride removal by aluminas before the linear portion of the fluoride removal versus gallonage curve had been reached. It is important especially with alumina adsorption columns to define the above mentioned region. The reason is improper switching of alumina adsorption columns* could result in a loss in efficiency. Information about the region before linear fluoride removal was reached would reduce the loss inefficiency, accordingly, test runs were scheduled. Since it was not known which of the available aluminas would be used in the final design configuration, six aluminas were chosen for a pseudo-kinetic** rate constant test runs. The rate adsorption constants and rate expressions derived would allow the prelinear region to be approximated closely. The proper switching of alumina columns could then be made based on the values for the items above. The experimental and mathematical methodology are given in the procedure section.

* It is anticipated two or more alumina columns will be needed to allow a regeneration cycle to be performed, especially if pH adjustment used.

** pseudo-kinetic or apparent rate; the rate of adsorption is actually much faster.

EXPERIMENTAL PROCEDURE

The items needed to determine a kinetic rate adsorption constant and a rate expression are the initial concentration (C_{a0}) and the concentrations (C_a) at set elapsed times (t). The generalized rate expression is $+\tau A = \frac{-dC_a}{dt}$, that is $+\tau f = \frac{-dC_a}{dt} = kf(C_a)$ with τf the pseudo-kinetic rate of adsorption; C_a the concentration at time t. The intergrated rate expression is then $\int dC_a/f(C_a) = -k \int dt$ with k the kinetic rate constant and t the elapsed time. Temperaure, pressure and alumina dosage were maintained constant with time of contact being varied. The alumina dosage was selected so that inter-ionic competition would be minimized between fluoride ions.

To find C_{a0} and C_a at t each rate test was done in the following manner:

- (1) Eight jars received 5 grams of the alumina being tested with a ninth jar set aside for a control;
- (2) The nine jars were filled with 800 ml of Calgon plant effluent water, placed in a constant temperature bath with agitators started;
- (3) Each hour a jar was removed and immediately filtered to 'stop' the adsorption action of the alumina, the control (blank) was filtered with the eight hour elapsed time sample;
- (4) Fluoride concentration and pH measurements were found on the samples and recorded along with elapsed time for the sample.

MATHEMATICAL PROCEDURE

Defining r_F as the apparent rate of disappearance of fluoride ion, C_F as the concentration of fluoride ion in solution and t as the time,

the apparent kinetic rate is given by $\frac{-dC_F}{dt} = +r_F$ for the reduction

of fluoride ion; this can also be written $\frac{-dC_F}{dt} = kf(C_F)$. The

equations given above are the generalized rate expressions, however, in order to obtain the integrated rate expression for predicting the adsorption of fluoride ions from solution, $f(C_F)$ must be found.

Rearranging the pseudo-kinetic rate expression gives $\frac{-dC_F}{f(C_F)} = kdt$ so that

the integrated rate expression can be found, when $f(C_F)$ known, by integration. One method is to assume $f(C_F)$ has the form C_F^N where $N = 0, 1/G, 1, G$ (G = real number) which limits the form of the integrated pseudo-kinetic rate expression to four forms. The four integrated pseudo-kinetic rate expressions are then:

(1) $C_{ao} =$ initial concentration and $C_a =$ concentration at time t .

$(C_a - C_{ao}) = -kt + I_c$ (I_c - constant of integration),

(2) $G(C_a^{1/G} - C_{ao}^{1/G}) = -kt + I_c$,

(3) $\ln(C_a/C_{ao}) = -kt + I_c$ and

(4) $1/G(C_a^{-G+1} - C_{ao}^{-G+1}) = -kt + I_c$

Now C_{ao} (the initial concentration) is a constant and the C_{ao} terms ($C_a - C_{ao}^{1/n}$) are therefore constant and can be represented by K_c (a constant term).

The four pseudo-kinetic rate expressions then become (after substitution and rearrangement):

$$(1) C_a = K_c + I_c - kt,$$

$$(2) G C_a^{1/G} = K_c + I_c - kt,$$

$$(3) \ln C_a = K_c + I_c - kt, \text{ and}$$

$$(4) \frac{1}{G} C_a^{-G} + \frac{1}{G} = K_c + I_c - kt.$$

Further combining the constants K_c and I_c to give a new constant $J_c = K_c + I_c$ renders the four pseudo-kinetic rate expressions in the final forms:

$$(1) C_a + J_c - kt,$$

$$(2) G C_a^{1/G} = K_c - kt,$$

$$(3) \ln C_a = J_c - kt, \text{ and}$$

$$(4) \frac{1}{G} C_a^{-G} + \frac{1}{G} = J_c - kt.$$

The problem now becomes one of selecting one of the above equations which represents the best fit to the C_a versus t plot. To select the best fit, the tabulated data was taken to MISO and analyzed via a modified simple regression program. This modified simple regression program calculated the correlation coefficient*, residuals, plotted the equation selected from the regression analysis, gave the 95% confidence bands for the linear case, and gave the $k G$ and I_c values. Since the aluminas are constrained to follow the same rate mechanism (by physical chemistry laws), it was expected one $f(C_a)$ would be found which would yield a high correlation coefficient for all the aluminas.

* Correlation coefficient (R^2) = 1.00 - direct correlation ($X = y$), excellent fit; $R^2 = -1.00$ - inverse correlation ($1/x = y$), excellent equation fit; $R^2 = 0.0$ - no correlation, R^2 between 0.0 and +1.00 - partial correlation with stronger correlation as $R^2 \rightarrow \pm 1.00$.

DATA AND RESULTS OF REGRESSION ANALYSIS

The concentrations of fluoride ion found for each elapsed time for the six aluminas tested are given in Table I below:

TABLE I: CONCENTRATION OF FLUORIDE ION VERSUS ELAPSED TIME FOR SIX SELECTED ALUMINAS

ALUMINA Elapsed Time Hours	MCB (Crushed) (Spheres)	Alcoa	Alcoa	Kaiser	Kaiser	Kaiser
		F-1 (Regenerated)	F-1 (Virgin)	A-300 (Ungraded)	A-201 (Spheres)	8 Mesh (Spheres)
1	2.69	3.08	2.52	1.48	3.35	3.12
2	2.40	2.92	1.97	0.978	3.26	2.94
3	2.00	2.83	1.84	0.780	3.18	2.86
4	1.68	2.75	1.49	0.778	3.12	2.48
5	1.46	2.73	1.43	0.766	3.04	2.24
6	1.02	2.70	1.41	0.729	3.02	2.17
7	1.00	2.60	1.28	0.608	3.00	2.15
8	0.907	2.59	1.19	0.560	2.95	1.69
8 (Blank) (initial Concen)	3.60	3.71	3.62	3.60	3.60	3.74

The regression analysis was initially performed with C_{ao} (the initial concentration of fluoride ion) included. Two conclusions were drawn from an analysis of the regression calculations :

- (1) overall $f(C_a)$ could take any of the four forms offered previously
- (2) the spheres all had $C_a = K_e \exp(-kt)$ as the 1st or 2nd best correlation.

The initial regression results with C_{ao} included are given in Figures 1-6. The plots of C_a vs. $K_e \exp kt$ for the six aluminas given in Figures 7-12.

When it comes to adsorption, the aluminas are chemically the same but physically the aluminas are different. The aluminas fall into two physical groups, spheres and granulated powders. The great difference in immediate surface area was postulated as the primary reason the spheres followed a \ln concentration (or exponential kt) form while the powders seemed to follow poorer formulations. In order to determine the behavior of the aluminas without the effect of large initially available surface area versus small initially available surface area, which occurs during the start-up of the tests, the zeroeth and first hour concentrations were deleted from the granulated powder regression analyses. Also to show that the small surface of the spheres had very little effect on the correlation coefficient, thus the fit of the equation, the zeroeth hour (initial concentration) was deleted and regressions analysis done. The plots and correlation coefficient for a minimized surface effect on the granulated powders is given in Figures 13-15 while the plots and correlation coefficients to show the minuscule surface effect on the spheres is given in Figures 16-18. As can be seen from Figures 13-15 the pseudo-kinetic rate expression takes on the form $C_a = K_e \exp (kt)$ with good correlation when the surface effect minimized. Several equations were tried in order to find the apparent kinetics for the surface area effect for the granulated powders and thus generate a predictive curve. The equation having the highest consistent correlation was $\sqrt{C_a} = K_e t^k$. The plots and correlation coefficients generated using the above equation are given in Figures 19-21. As is seen from the high correlation coefficients the above expression simulates the surface area effects quite well. By now combining the results of the previous plots, it is seen the spherical shaped aluminas fluoride removal can be simulated by $C_a = K_e \exp (kt)$ integrated

rate expressions up to constant removal rate region and the granulated powder by $\sqrt{C_a} = K_e t^k$ 0-2 hours then $C_a = K_e \exp(kt)$ from 2 hours to constant removal rate region start. This is shown below in Figures 22 and 23 for spherical and granulated power aluminas, respectively.

FIGURE 22: PREDICTIVE FLUORIDE ION CONCENTRATION IN ALUMINA COLUMN VS ELAPSED TIME MODEL

FIGURE 23: PREDICTIVE FLUORIDE ION CONCENTRATION IN ALUMINA COLUMN VS ELAPSED TIME MODEL

CONCLUSIONS

The predictive models for finding fluoride concentration during the

critical start-up (switch-over times) allow the alumina column process to be more closely monitored. Using some of the Ruebel and Hager, Inc. start-up data further verification of these predictive models was made. The plots of \ln concentration vs Time and the correlation coefficients are given in Figures 24 and 25. NOTE: $\ln C_a = K_e + kt$ is equivalent to $C_a = K_e \exp(kt)$. As is seen the correlation coefficients are good considering the surface area effect was not considered in these analyses. These pseudo-kinetic rate test results are not completely conclusive without several repetitions of the tests made on the aluminas. A further pseudo-kinetic rate test coupled with column test should be made to enable fluoride removal in alumina columns to be predicted by the mathematical models found.

FIGURE 1: REGRESSION (f (CA) vs kt) on ALCOA F-1 (VIRGIN)

SELECT BEST FIT

EQUATION	A	B	RES ERROR	R-SQUARE	MAX DEVIATION
$Y = A + Bx$	0.25505		1.68905	-6.02188	2.26495
$Y = A + Bx^2$	2.39714	-0.16798	0.03164	0.86194	0.29083
$Y = A + B\exp(Bx)$	2.48048	-0.09819	0.02101	0.90832	0.27150
$Y = 1/(A + Bx)$	0.37589	0.05950	0.01312	0.94277	0.22321
$Y = A + B/x$	1.14479	1.46133	0.01415	0.93826	0.20810
$Y = A + B\log(x)$	2.46763	-0.62341	0.00481	0.97900	0.11340
$Y = A + Bx^3$	2.54568	-0.35289	0.00389	0.98303	0.11245
$Y = x/(A + Bx)$	-0.45532	0.79833	0.05395	0.76455	0.39533

EQUATION "Y = A + Bx HAS MAXIMUM R-SQUARE

EQUATION "Y = A + Bx HAS MINIMUM MAXIMUM ABSOLUTE RESIDUAL

FIGURE 2: REGRESSION (f (CA) US kt) on ALCOA F-1 (REGENERATED)

SELECT BEST FIT

EQUATION A B

$$Y = A * X \quad 0.54564$$

$$Y = A + B * X \quad 3.08714 \quad -0.07179$$

$$Y = A * EXP(B * X) \quad 3.09568 \quad -0.02544$$

$$Y = 1 / (A + B * X) \quad 0.32198 \quad 0.00904$$

$$Y = A + B / X \quad 2.61403 \quad 0.50207$$

$$Y = A + B * LOG(X) \quad 3.68291 \quad -0.23238$$

$$Y = A * X^B \quad 3.08871 \quad -0.08172$$

$$Y = X / (A + B * X) \quad -0.06135 \quad 0.38086$$

$$Y = A + B * LOG(X) \quad 0.00394 \quad 0.87316$$

EQUATION $Y = A + B * LOG(X)$ HAS MAXIMUM R-SQUARE

EQUATION $Y = A + B * LOG(X)$ HAS MINIMUM MAXIMUM ABSOLUTE RESIDUAL

RES ERROR

2.67071

0.00218

0.00195

0.00174

0.00324

0.00067

0.00074

0.00394

0.87316

R-SQUARE

-85.04086

0.92970

0.93711

0.94380

0.89556

0.97838

0.97631

0.87316

0.04461

MAX DEVIATION

2.53436

0.06464

0.06209

0.05903

0.09575

0.04083

0.09752

FIGURE 3: REGRESSION (f (CA) US kt) on MCB SPHERES (8 x 14)
SELECT BEST FIT

EQUATION A	B	RES ERROR	R-SQUARE	MAX DEVIATION
$Y = A + B * X$ 0.23474		2.26210	-3.27508	2.45526
$Y = A + B * X$ 2.85754	-0.26954	0.02059	0.96109	0.22032
$Y = A * EXP(B * X)$ 3.25475	-0.16843	0.00757	0.98570	0.16478
$Y = 1 / (A + B * X)$ 0.19413	0.11385	0.06425	0.87857	0.55698
$Y = A + B * X$ 0.95566	2.02795	0.11508	0.78251	0.43036
$Y = A + B * LOG(X)$ 2.88529	-0.93595	0.02349	0.95560	0.19529
$Y = A * X^1/B$ 3.21502	-0.56250	0.08371	0.84181	0.52502
$Y = X / (A + B * X)$ -0.73398	0.95580	0.74589	-0.40963	1.81831

EQUATION $Y = A * EXP(B * X)$ HAS MAXIMUM R-SQUARE

EQUATION $Y = A * EXP(B * X)$ HAS MINIMUM MAXIMUM ABSOLUTE RESIDUAL

FIGURE 4: REGRESSION (f (CA) VS kt) on KAISER A-201 (SPHERES)
SELECT BEST FIT

EQUATION	A	B	RES ERROR	R-SQUARE	MAX DEVIATION
$\gamma = A + B*x$	0. 53632		3.13162	-120.78396	2.81368
$\gamma = A + B*x$	3. 37714	-0. 05964	0. 00081	0. 96836	0. 04036
$\gamma = A*EXP(B*x)$	3. 38473	-0. 01912	0. 00071	0. 97252	0. 03939
$\gamma = 1/(A + B*x)$	0. 29469	0. 00614	0. 00062	0. 97606	0. 03838
$\gamma = A + B/x$	2. 95507	0. 45237	0. 00511	0. 80121	0. 11161
$\gamma = A + B*LOG(x)$	3. 38305	-0. 20693	0. 00100	0. 96116	0. 05276
$\gamma = A*x^1B$	3. 38936	-0. 06594	0. 00117	0. 95445	0. 05506
$\gamma = x/(A + B*x)$	-0. 04545	0. 33775	0. 00581	0. 77423	0. 11142
EQUATION $\gamma = 1/(A + B*x)$ HAS MAXIMUM R-SQUARE					
EQUATION $\gamma = 1/(A + B*x)$ HAS MINIMUM MAXIMUM ABSOLUTE RESIDUAL					

FIGURE 5: REGRESSION (f (CA) US kt) on KAISER 8 MESH (SPHERES)

SELECT BEST FIT

EQUATION	A	B	RES ERROR	R-SQUARE	MAX DEVIATION
----------	---	---	-----------	----------	---------------

$$Y = A*X$$

$$0.39358$$

$$Y = A + B*X$$

$$3.32786$$

$$-0.19369$$

$$Y = A*EXP(B*X)$$

$$3.47086$$

$$-0.08079$$

$$Y = 1/(A + B*X)$$

$$0.26684$$

$$0.03452$$

$$Y = A + B/X$$

$$1.99753$$

$$1.35025$$

$$Y = A + B*LOG(X)$$

$$3.31300$$

$$-0.64632$$

$$Y = A*X^B$$

$$3.42238$$

$$-0.26366$$

$$Y = X/(A + B*X)$$

$$-0.22025$$

$$0.49703$$

$$Y = A + B*X$$

$$0.47777$$

$$0.47777$$

EQUATION $Y = A + B*X$ HAS MAXIMUM R-SQUARE

EQUATION $Y = A + B*X$ HAS MINIMUM MAXIMUM ABSOLUTE RESIDUAL

3.05211

-10.11350

2.72642

0.01202

0.95623

0.17798

0.01363

0.95035

0.17837

0.02133

0.92232

0.19822

0.09107

0.66837

0.47631

0.03351

0.87800

0.27901

0.04899

0.82161

0.30238

FIGURE 6: REGRESSION (f (CA) VS kt) on KAISER A-300 (UNGRADED)

SELECT BEST FIT

EQUATION A B RES ERROR R-SQUARE MAX DEVIATION

$$Y = A*X 0.12661 0.48200 -3.93601 1.35339$$

$$Y = A + B*X 1.28782 -0.10065 0.02673 0.72627 0.29283$$

$$Y = A*EXP(B*X) 1.32280 -0.11188 0.02166 0.77817 0.29722$$

$$Y = 1/(A + B*X) 0.69823 0.13298 0.01725 0.82336 0.27694$$

$$Y = A + B/X 0.50532 0.97005 0.00291 0.97019 0.06667$$

$$Y = A + B*LOG(X) 1.35293 -0.39082 0.00948 0.90287 0.14358$$

$$Y = A*X^B 1.38383 -0.41384 0.00521 0.94667 0.09828$$

$$Y = X/(A + B*X) -1.06049 1.65694 0.01187 0.87843 0.19659$$

EQUATION $Y = A + B/X$ HAS MAXIMUM R-SQUARE

EQUATION $Y = A + B/X$ HAS MINIMUM MAXIMUM ABSOLUTE RESIDUAL

FIGURE 7: CA vs. KE exp (kt) - ALL POINTS INCLUDED

$A = 2.86125421388$
 $B = -0.123387635828$

R-SQUARE =
0.842140771894

RES ERROR
0.109493165176

MAX(CABS(CRESIDUAL))
0.758745786118

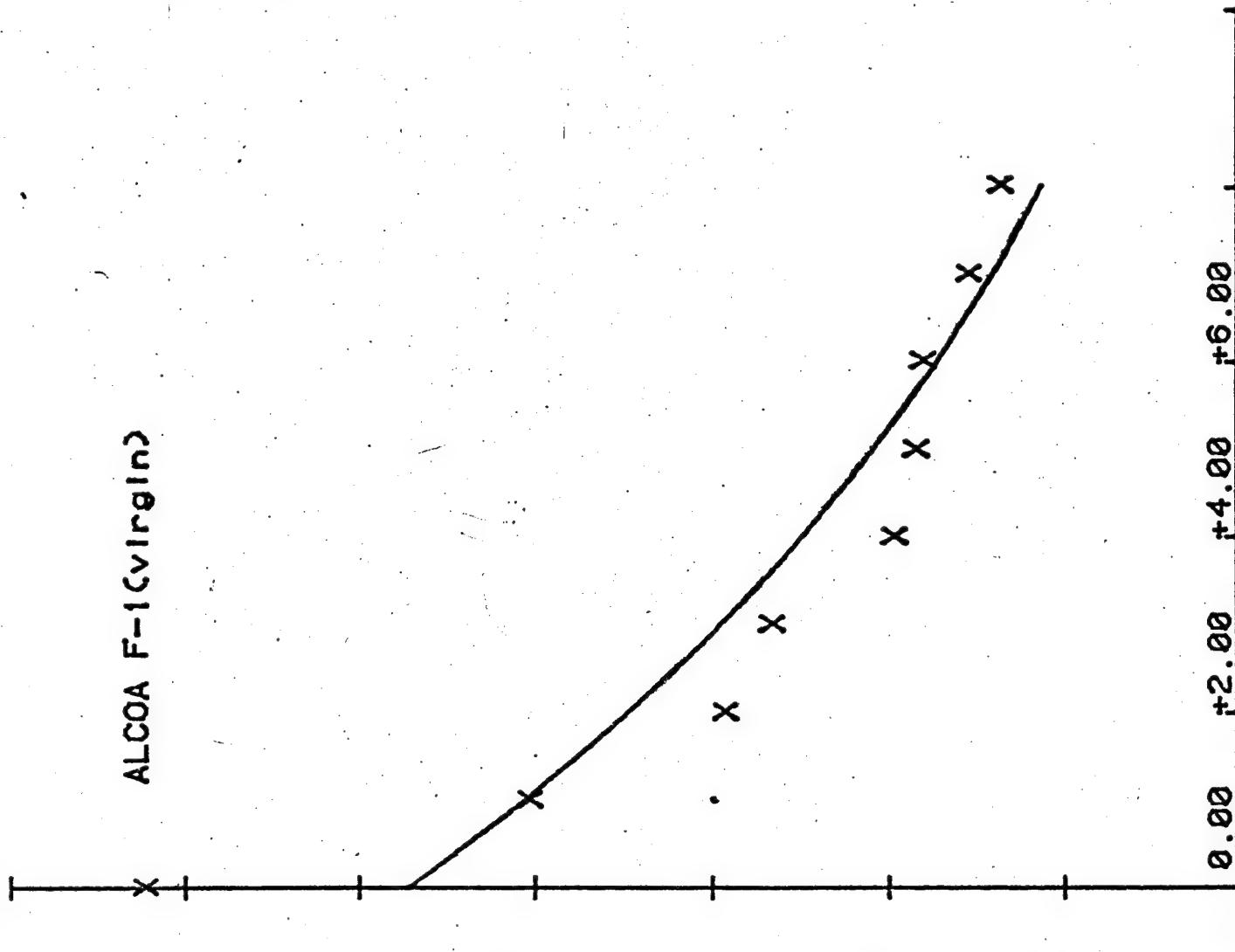


FIGURE 8: CA vs. KE exp (kt) - ALL POINTS INCLUDED.

ALCOA F-1 (regenerated)

$$A = 3.29984035992$$

$$+3.60$$

$$B = -0.0355755946531$$

$$+3.40$$

$$R^2 = 0.741570992133$$

$$RES. ERROR
0.0357107868396$$

$$MAX(CABS(CRESIDUAL))
0.410159640083$$

$$+3.00$$

$$+2.80$$

$$+2.60$$

$$0.00 \quad +2.00 \quad +4.00 \quad +6.00$$

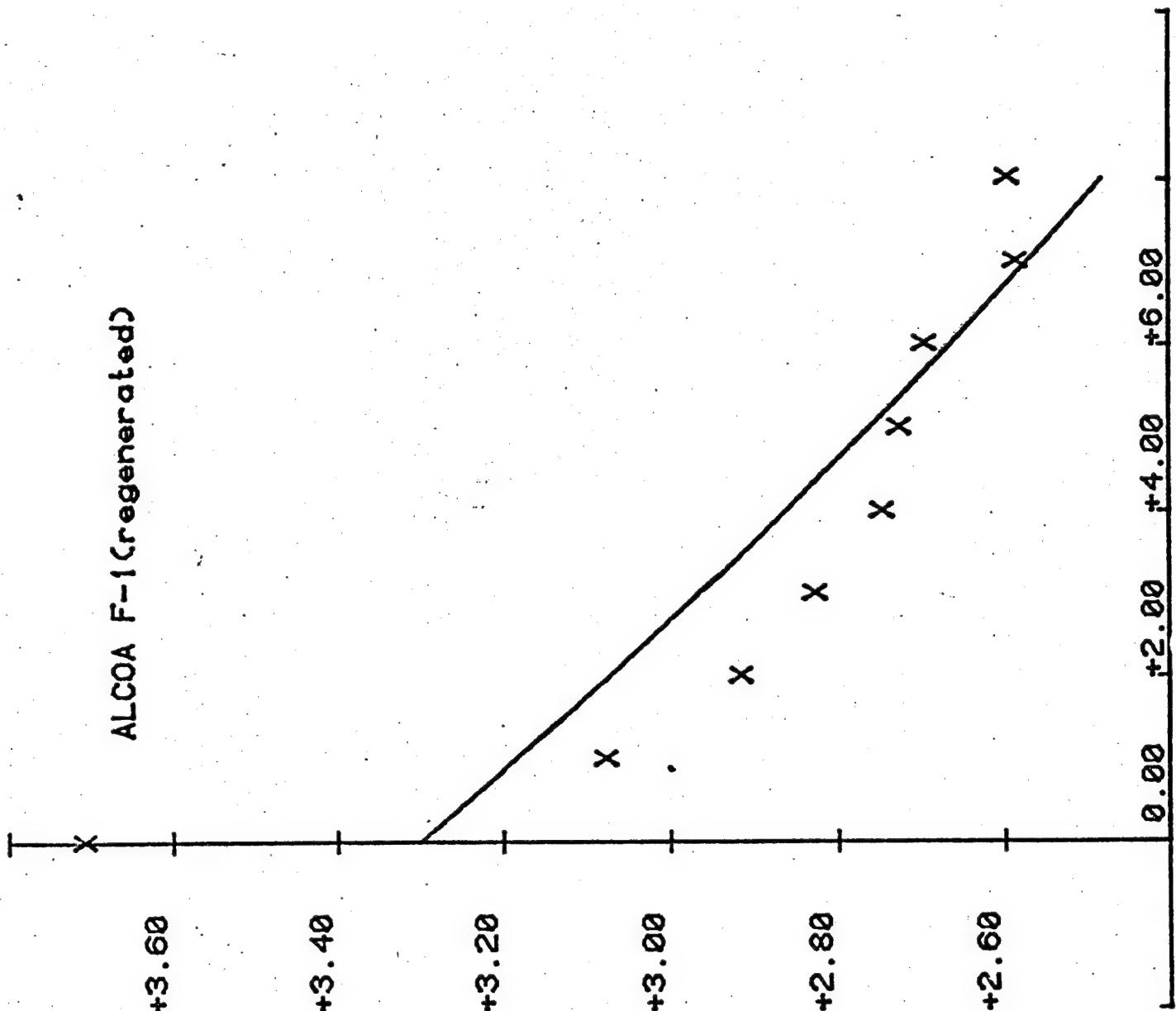


FIGURE 9: CA vs. KE exp (kt) - ALL POINTS INCLUDED

MCB (crushed spheres)

$$A = 3.38110489411$$

$$B = -0.175147554052$$

$$R^2 = 0.984083249635$$

$$RES. ERROR = 0.0149469129533$$

$$MAX(ABS(CRESIDUAL)) = 0.218895105895$$

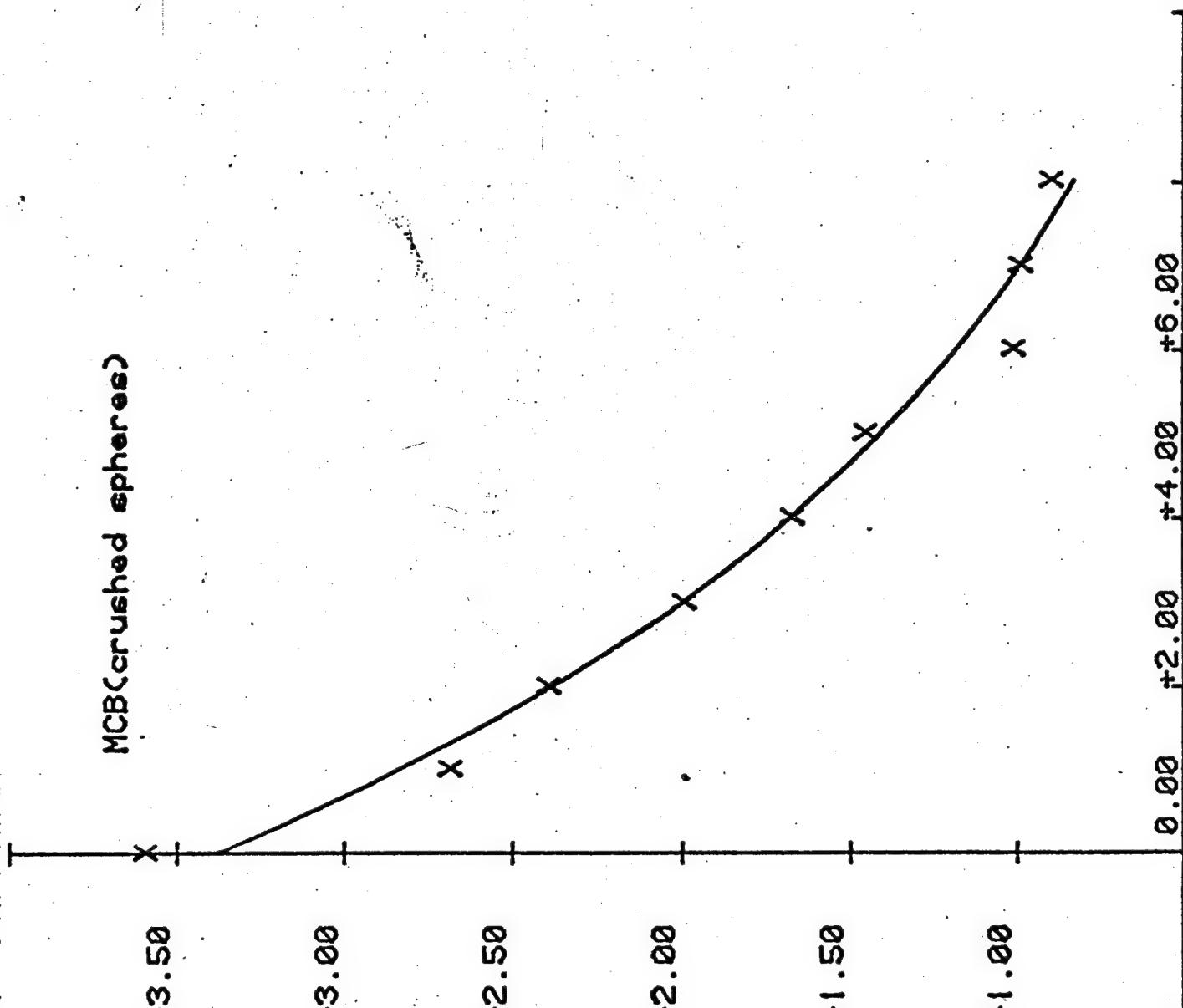


FIGURE 10: CA vs. KE exp (kt) - ALL POINTS INCLUDED.

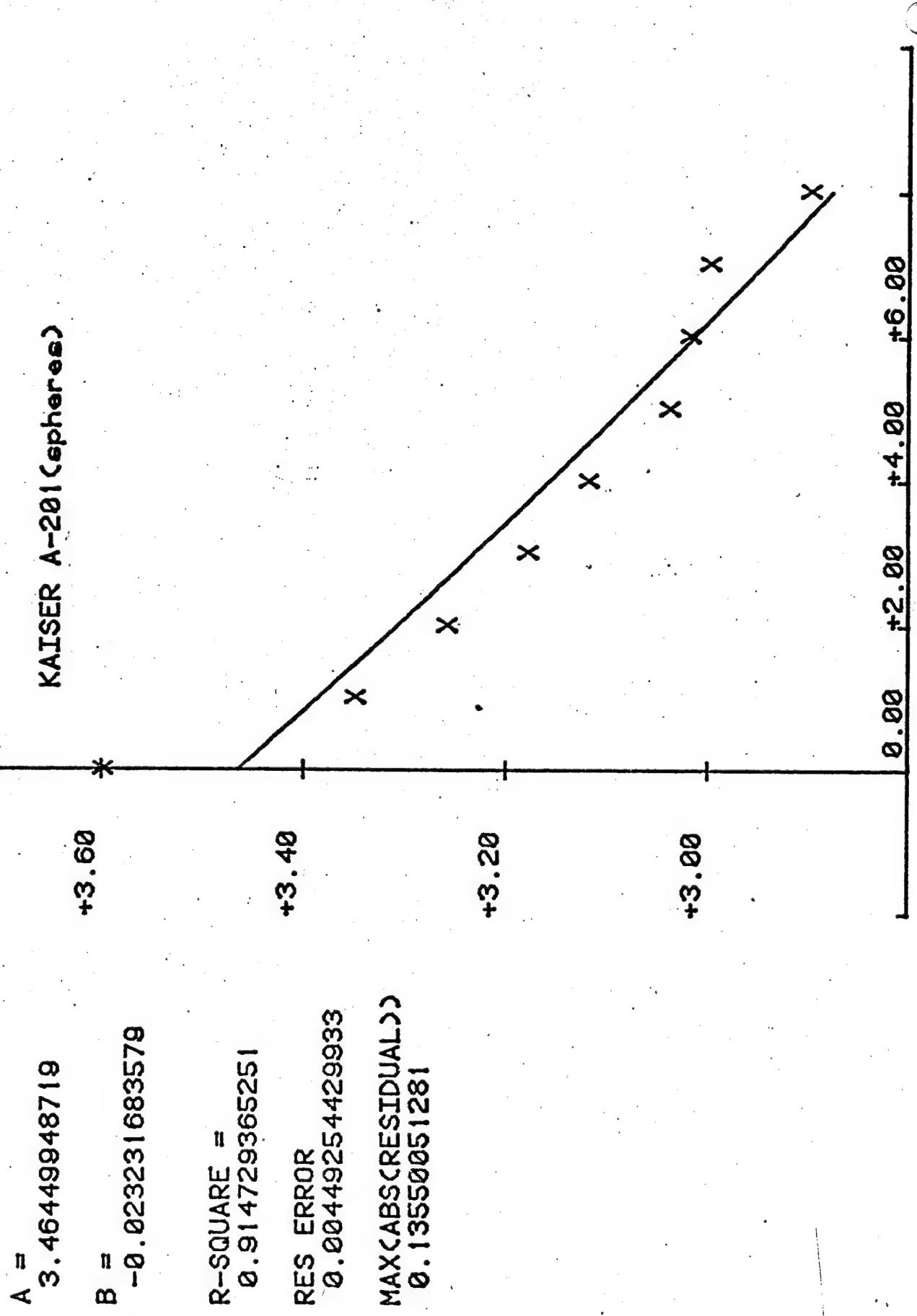


FIGURE 11: CA vs. KE exp (kt) - ALL POINTS INCLUDED.

$$A = 3.57018170149$$

$$B = -0.0857705732595$$

$$R^2 = 0.959037264707$$

$$RES. ERROR
0.01821489300007$$

$$MAX (ABS (RESIDUAL))
0.191414599056$$

KAISER 8 MESH (spheres)

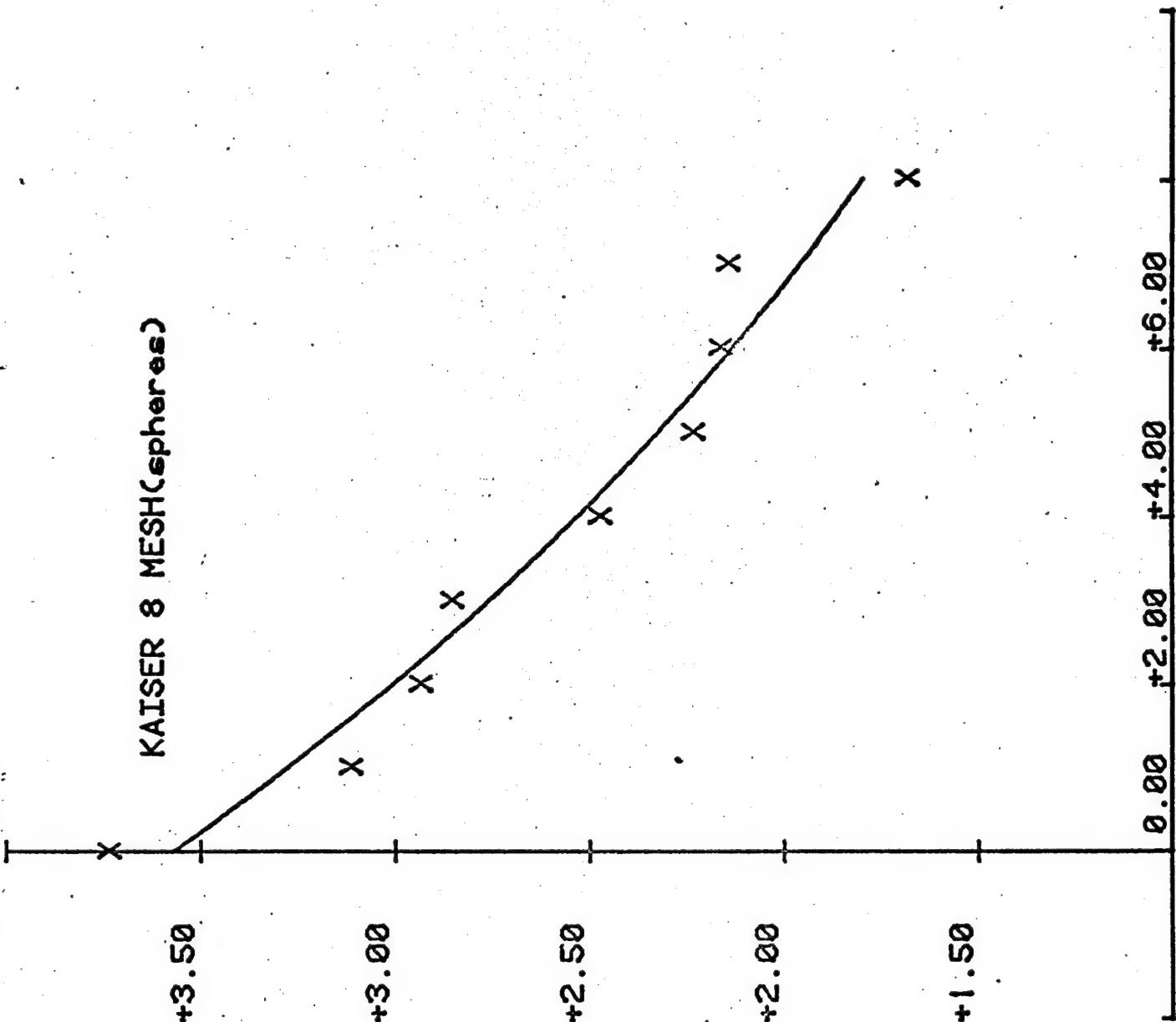


FIGURE 12: CA vs. KE exp (kt) - ALL POINTS INCLUDED.

KAISER A-300 (ungraded)

+3.50

$A = 1.322800092624$

$B = -0.111882177845$

R-SQUARE =
 0.778168813566

RES ERROR
 0.0216617737619

MAX(ABS(RESIDUAL))
 0.297218078377

+1.50

+1.00

+0.50

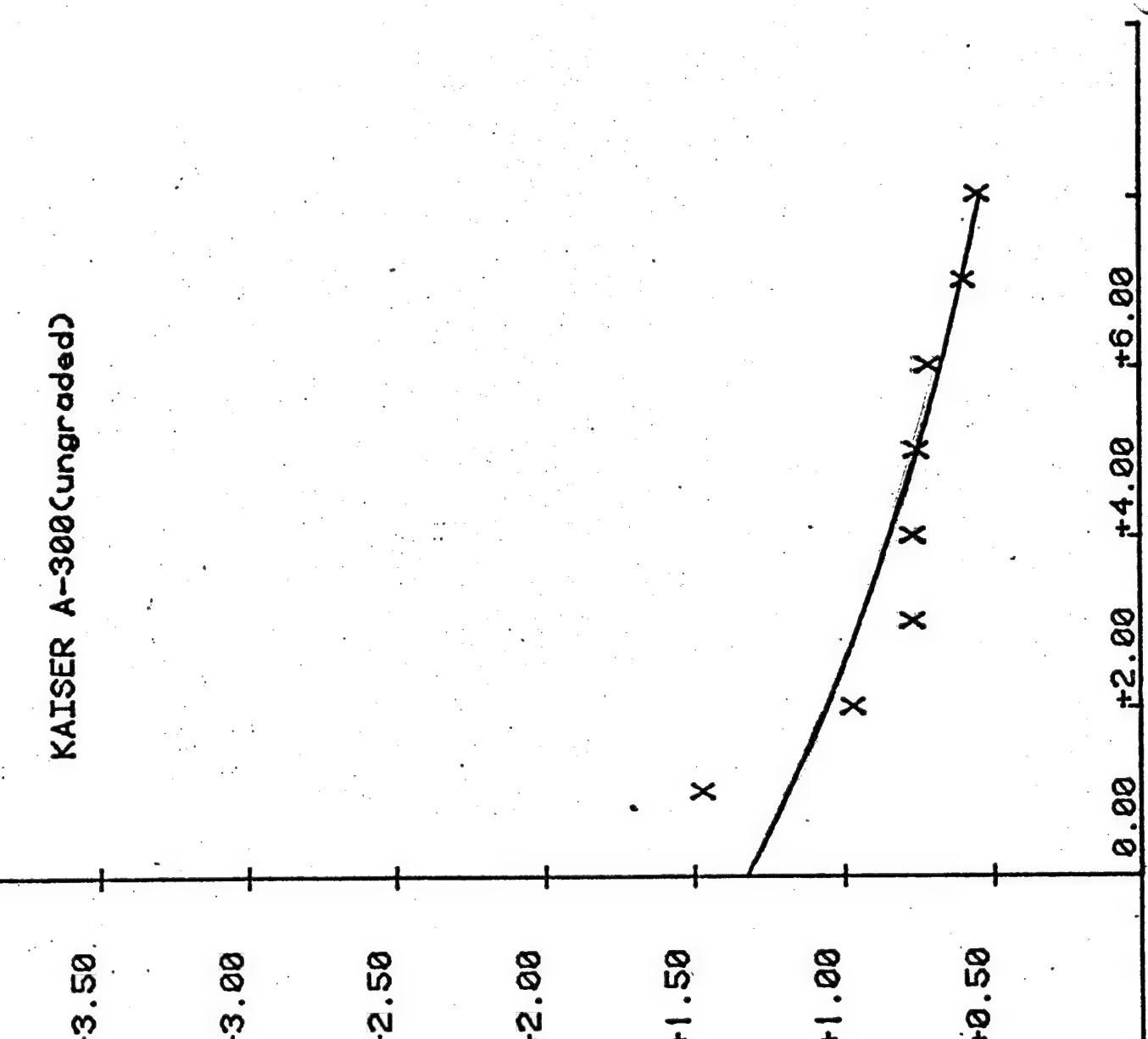


FIGURE 13:

ALCOA F-1 (Virginia)-SURFACE EFFECT MINIMIZED

$$A = 2.24957861183$$

$$B = -0.0819013610652$$

$$R-SQUARE = 0.932718132716$$

$$RES ERROR 0.00662553382235$$

$$MAXCABS(RESIDUAL) 0.131152750837$$

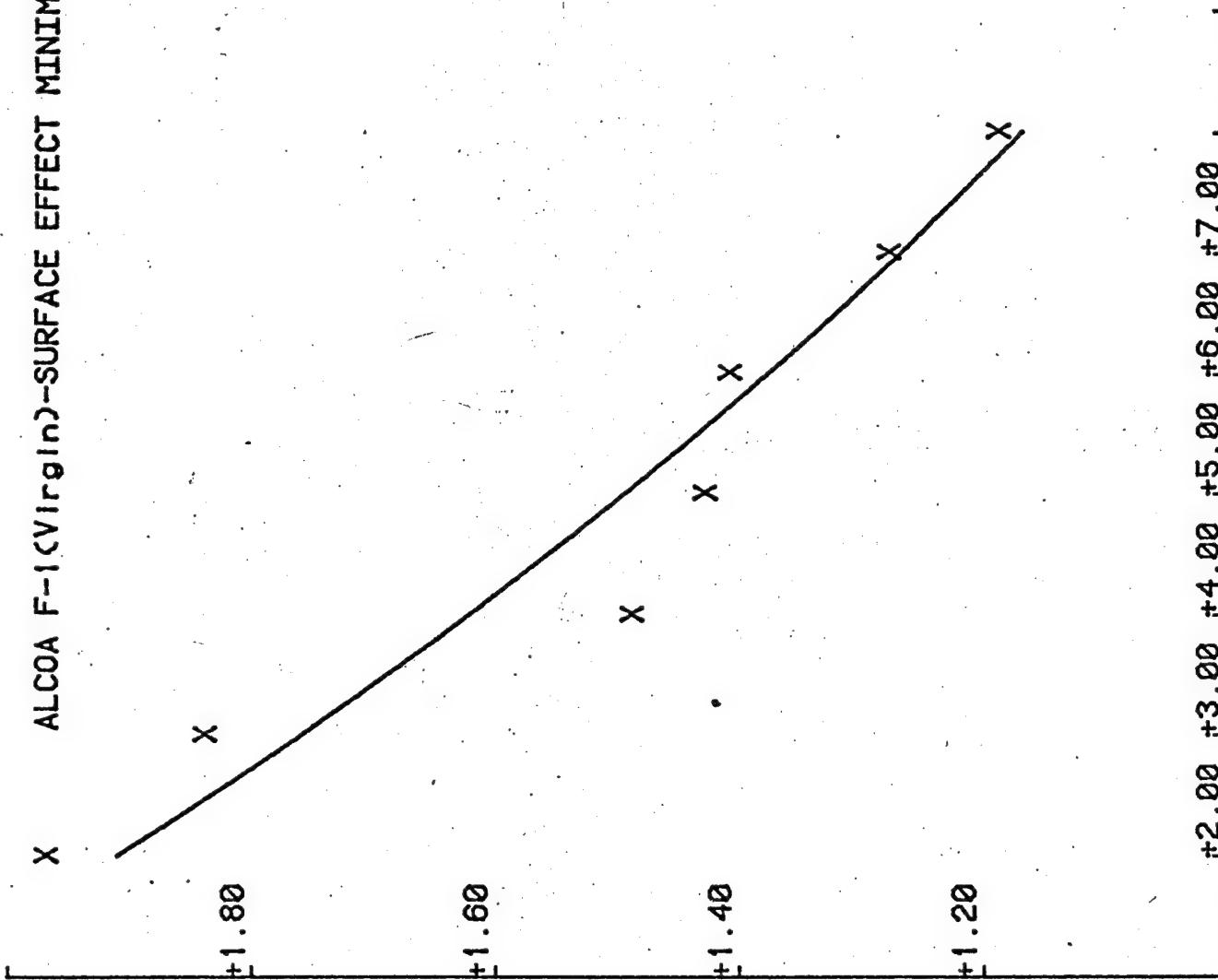


FIGURE 14:

ALCOA F-1 (Regenerated)-SURFACE EFFECT MINIMIZED

$$A = 3.00964505949$$

$$B = -0.0195591747725$$

$$R-SQUARE = 0.961163734239$$

$$RES ERROR 6.515615787E-4$$

$$MAX(CABS(CRESIDUAL)) 0.0331557681378$$

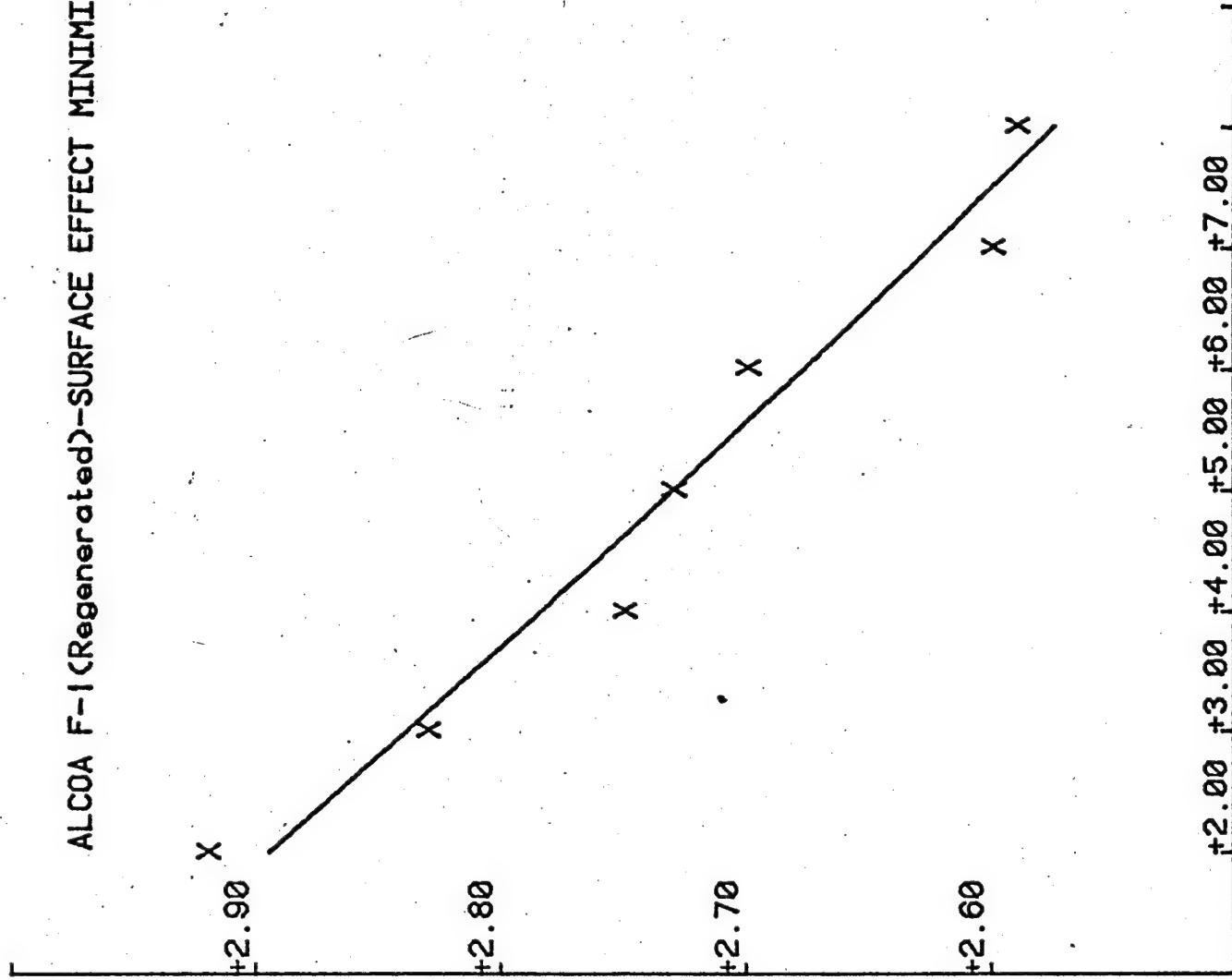


FIGURE 15:

KAI SER A-300 (UNGRADED) - SURFACE EFFECT MINIMIZED

$$A = 1.09155494399$$

$$B = -0.0798574830901$$

$$R-SQUARE = 0.880220957939$$

$$RES ERROR 0.00264130583489$$

$$MAX(ABS(RESIDUAL)) 0.0790147247008$$

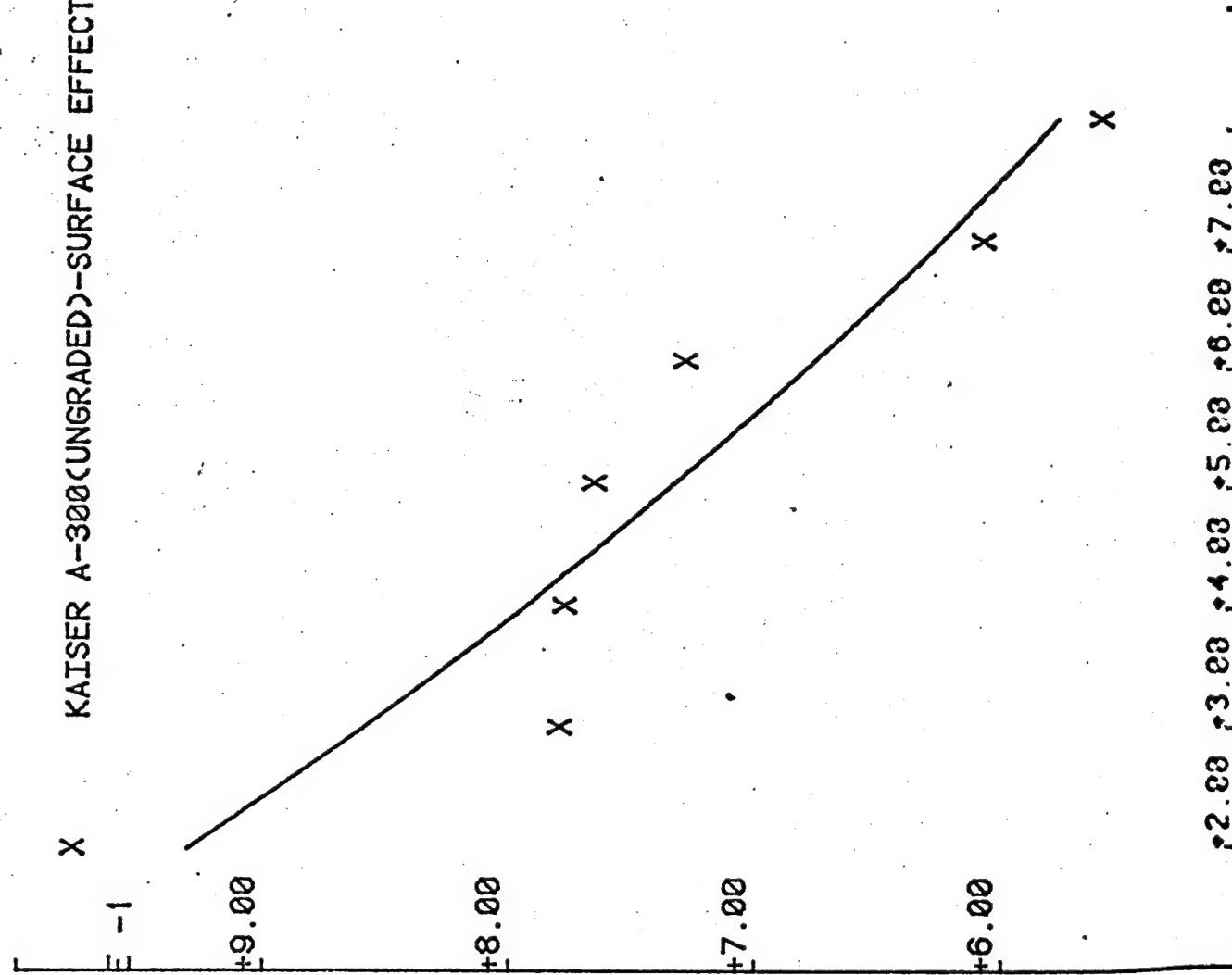


FIGURE 16: SURFACE AREA EFFECT ON KINETIC RATE EXPRESSION CORRELATION COEFFICIENT

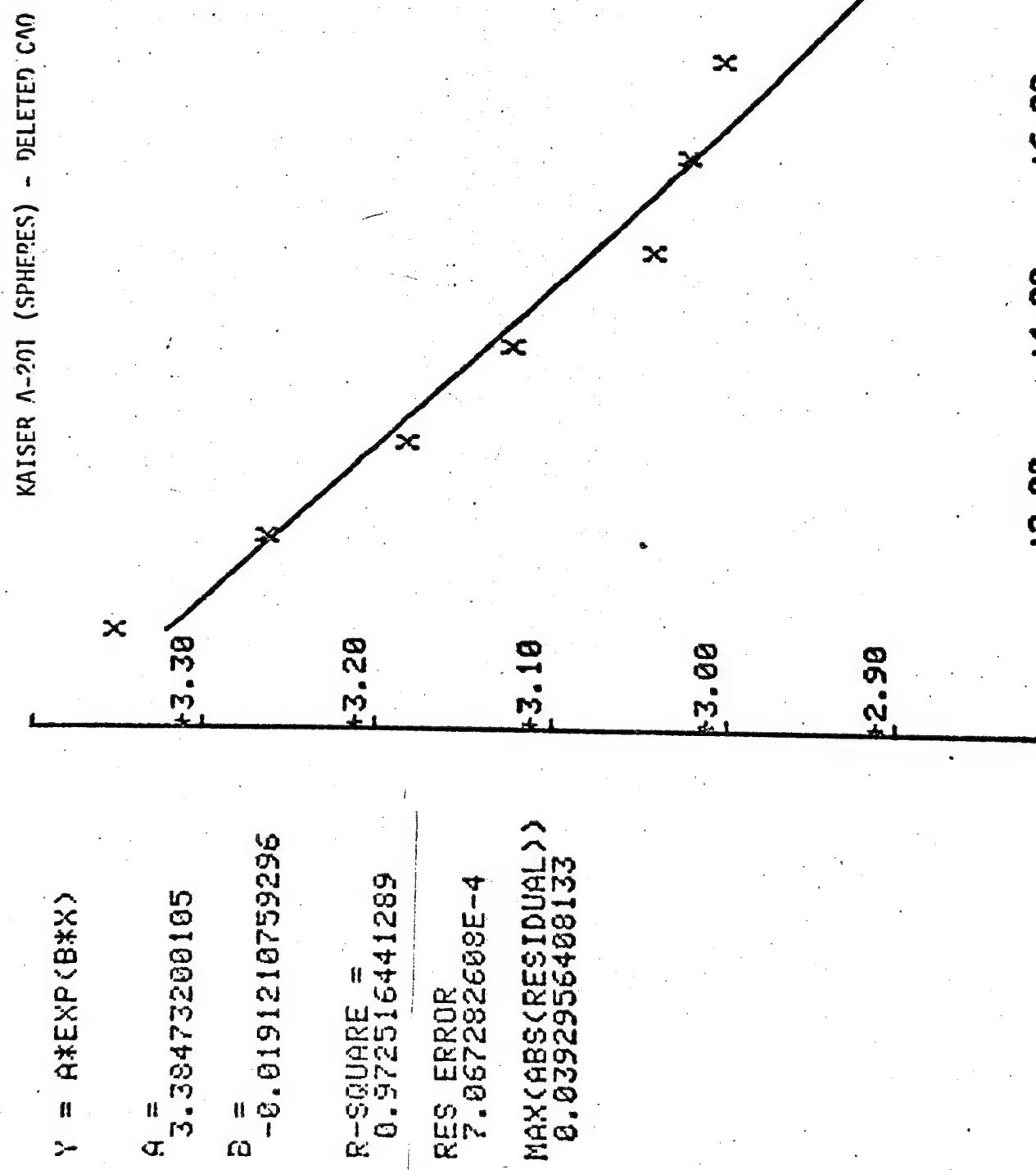
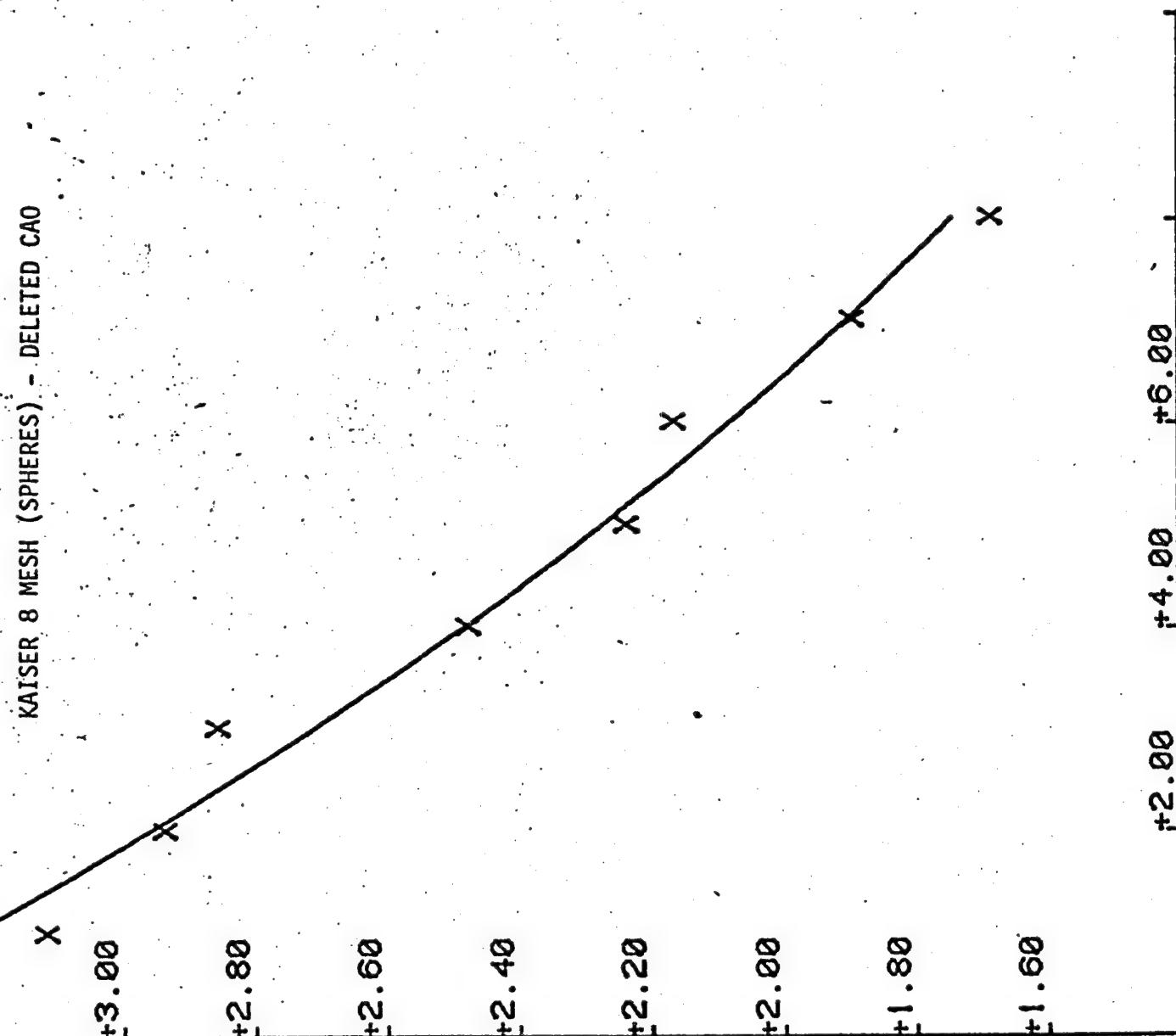


FIGURE 17: SURFACE AREA EFFECT ON KINETIC RATE EXPRESSION CORRELATION COEFFICIENT



=
3.53269823114

=
-0.0881497125267

-SQUARE =
0.974353713247

ES ERROR
0.00793154161634

MAX(CABSRESIDUAL))
0.148198712349

FIGURE 18: SURFACE AREA EFFECT ON KINETIC RATE EXPRESSION CORRELATION COEFFICIENT

MCB (CRUSHED SPHERES) - DELETED CAO

$y = A * EXP(B * x)$

$A = 3.25475071848$

$B = -0.168426343591$

R-SQUARE =
0.985782993755

RES. ERROR
0.00756506516408

MAX(ABS(RESIDUAL))
0.164780620419

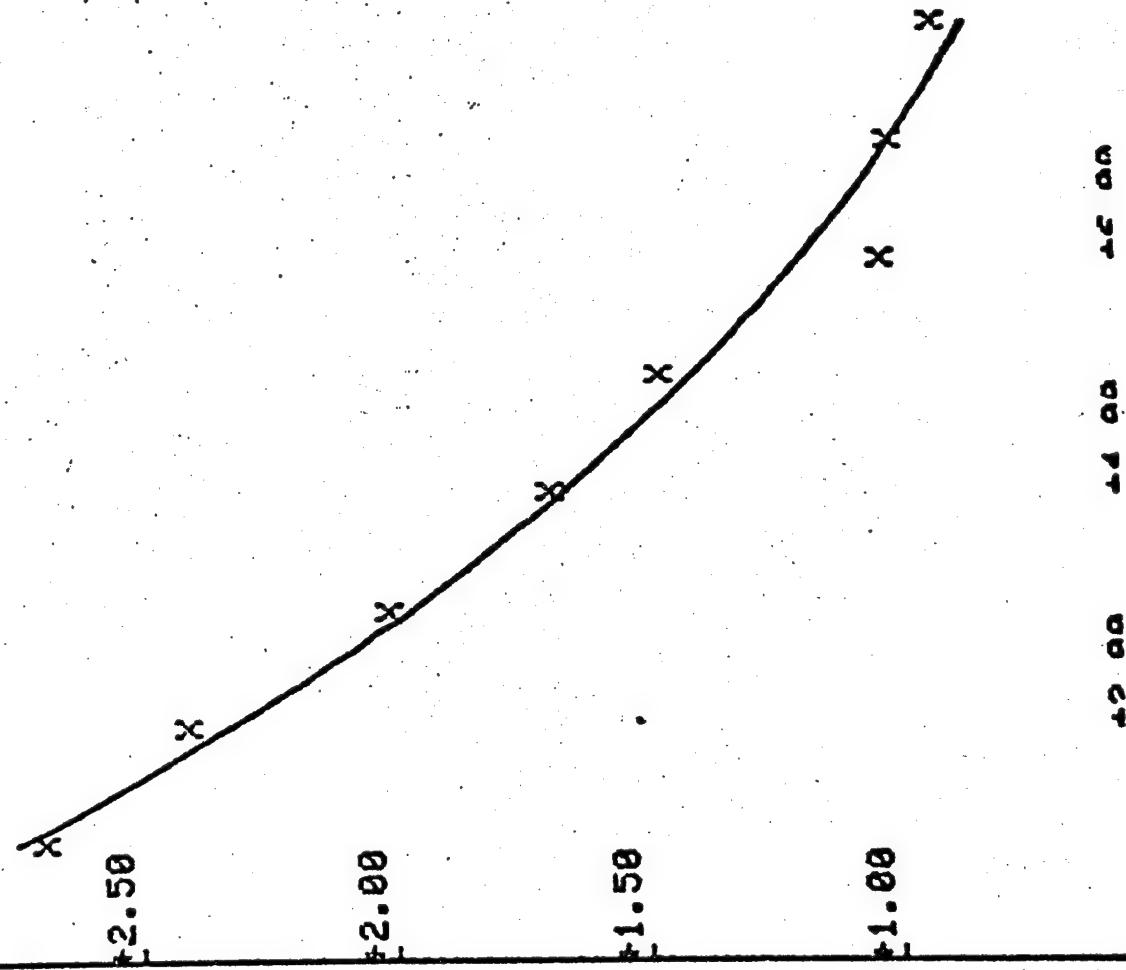


FIGURE 19:

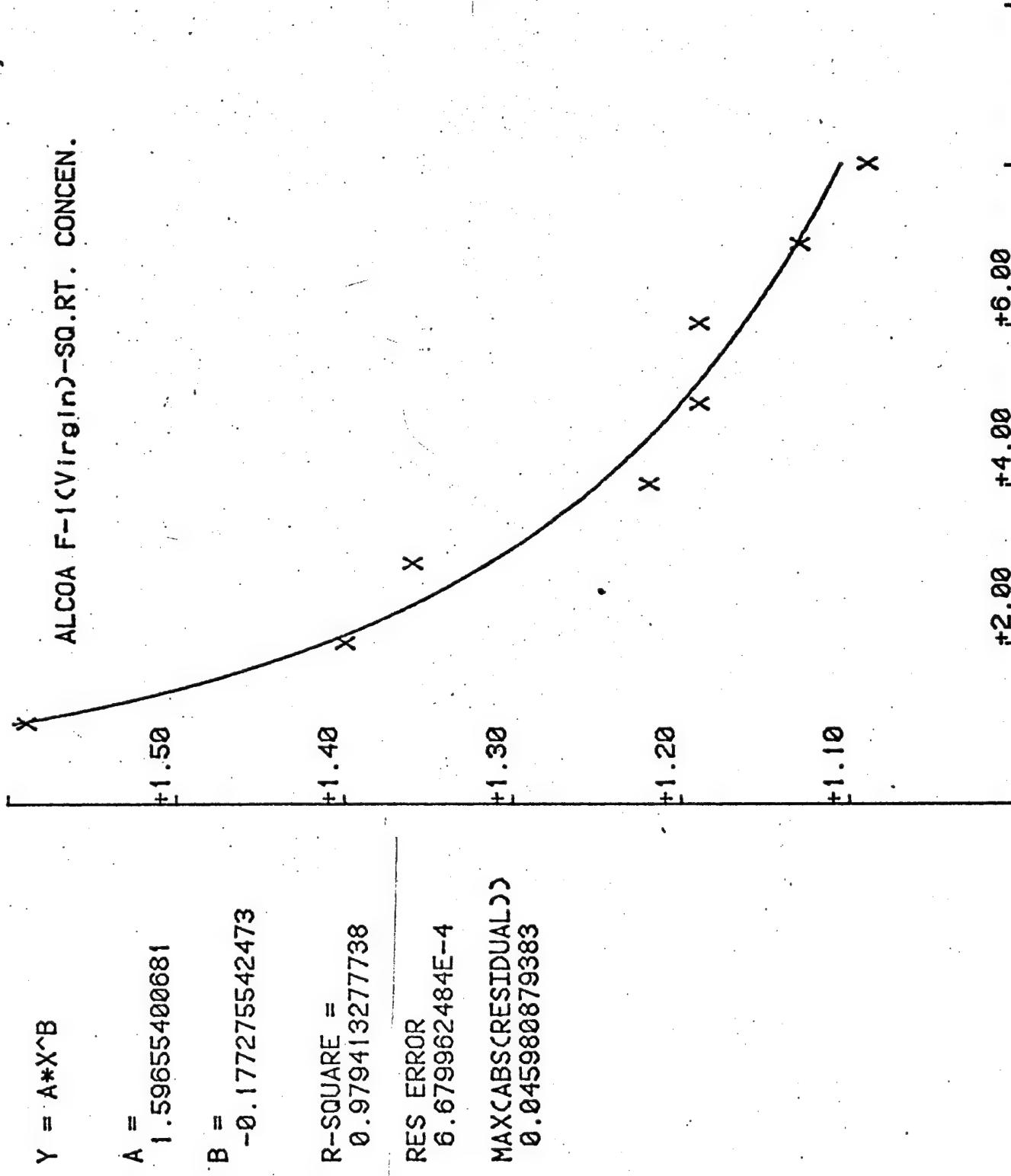


FIGURE 20:

$$Y = A \cdot X^B$$

$$A = 1.76160785782$$

$$B = -0.0428547039272$$

$$R-SQUARE = 0.98757451959$$

$$RES. ERROR 3.769062391E-5$$

$$MAX|ABS(RESIDUAL)| 0.0106633557477$$

ALCOA F-1 (Regenerated)-SQ.RT. CONCEN.

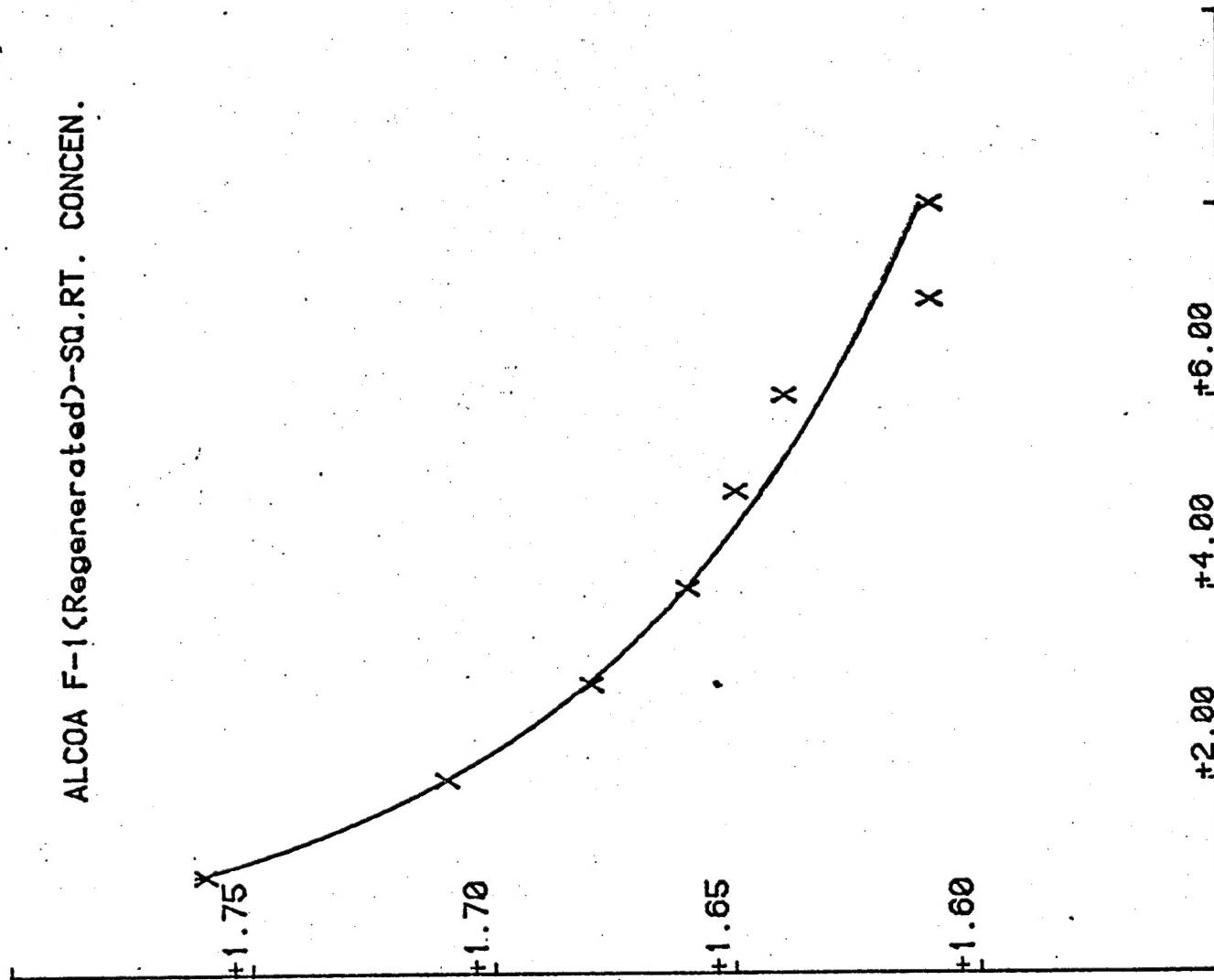


FIGURE 21:

Y = A*X^B
KAI SER A-300 (Ungraded) - SQ.RT. CONCEN.

$$A = 1.17623909209$$

$$B = -0.207245174192$$

$$R-SQUARE = 0.944371373405$$

$$RES. ERROR 0.00138003496857$$

$$MAX(ABS(CRESDUAL)) 0.0537302203461$$

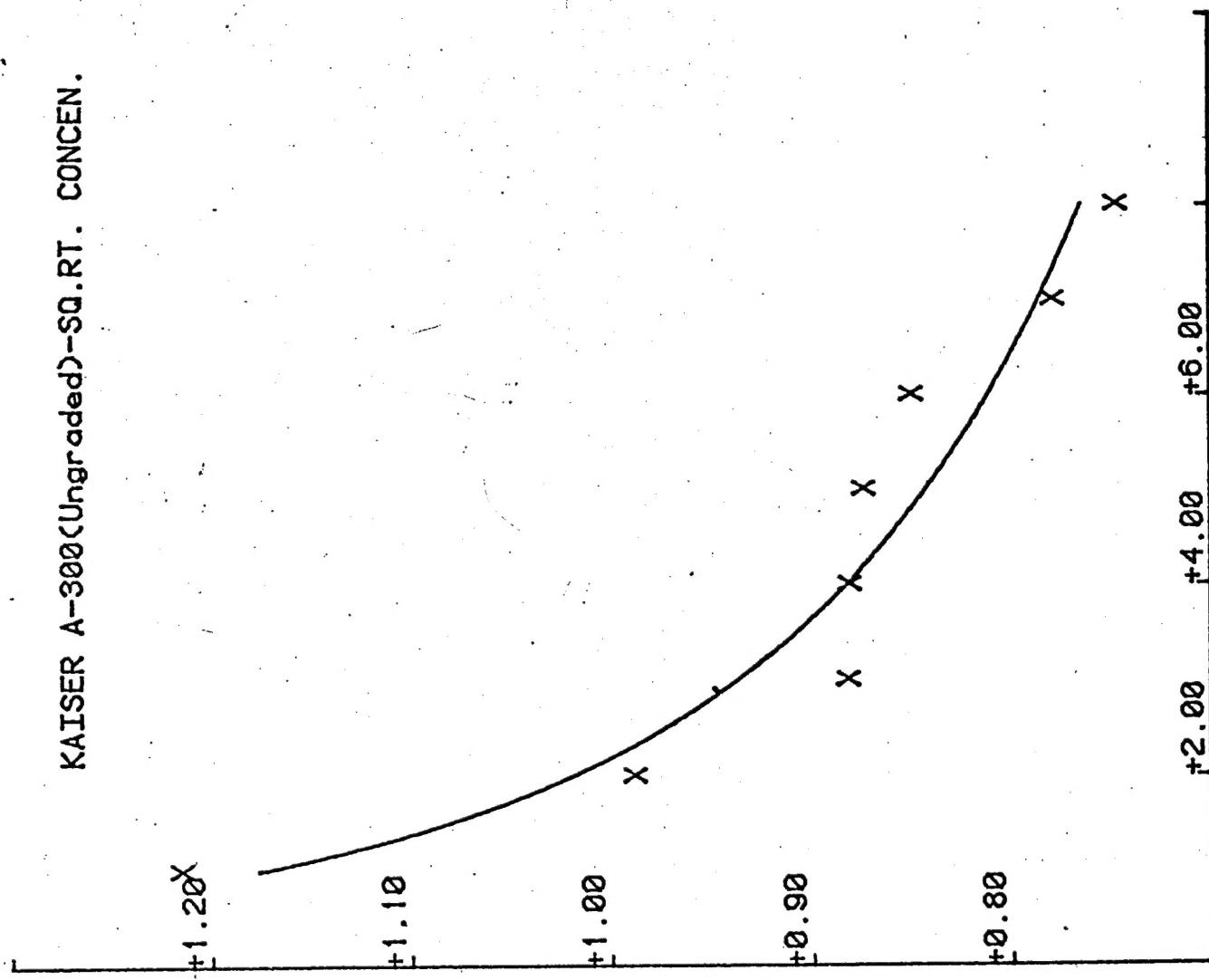


FIGURE 24:

ALCOA F-1 (Virginia)-R&H RUN at pH 7.72

$E = -1$

$A = 0.758141426723$

$+9.00$

$B = -0.0726143816953$

$R^2 = 0.909555764927$

$RES\ ERROR$
 $2.02368976E-4$

$MAX(ABS(CRESCIDUAL))$
 0.0161359584475

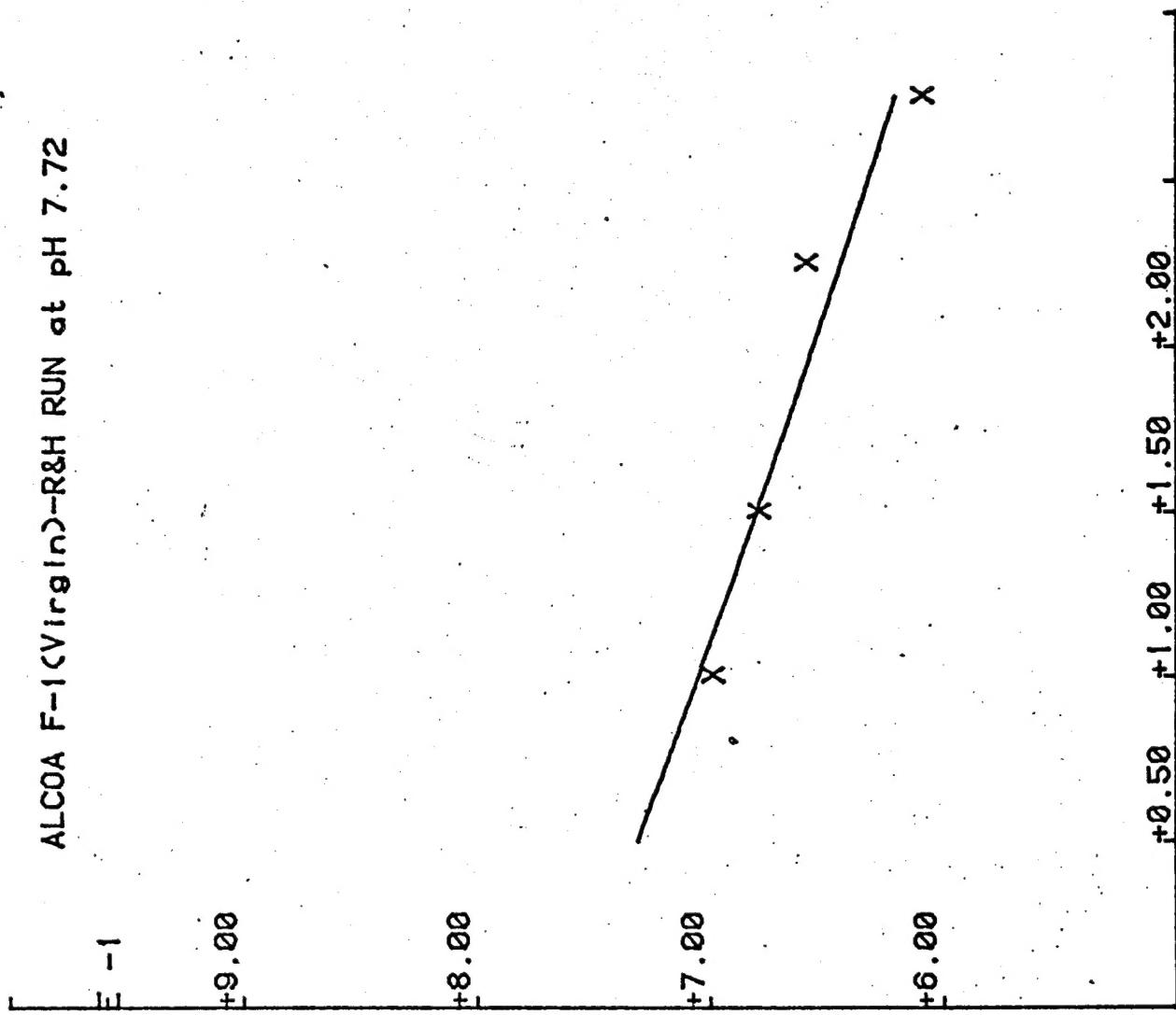


FIGURE 25:

$$Y = A + B*X$$

$$A = 1.434$$

$$B = -2.02285714286$$

$$R-SQUARE = 0.984640129417$$

$$RES ERROR 0.0174541428571$$

$$MAX(CABS(CRESIDUAL)) 0.140285714286$$

ALCOA F-1 (Regenerated)-R&H RUN at pH 11.3
(Ln Concentration)

